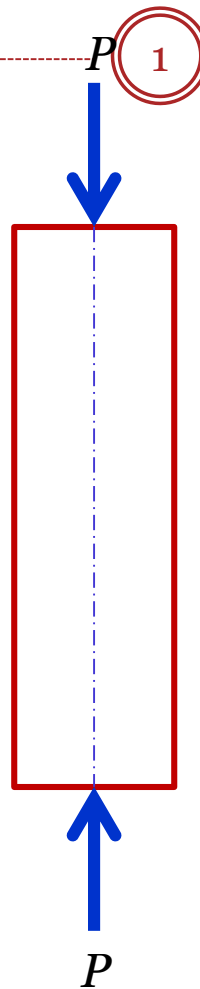


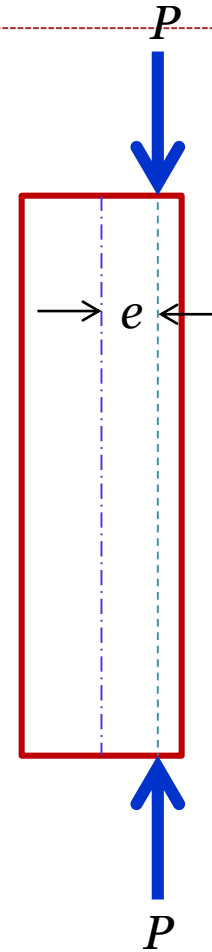
Design of Short Columns

- Reinforced Concrete (RC) short columns are divided into two categories:

- Columns with a purely Axial load (no moment)
- Columns carrying eccentric loads

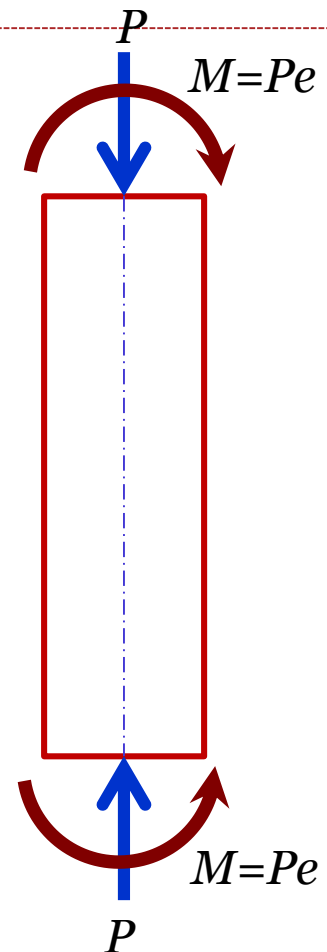


Axially loaded column



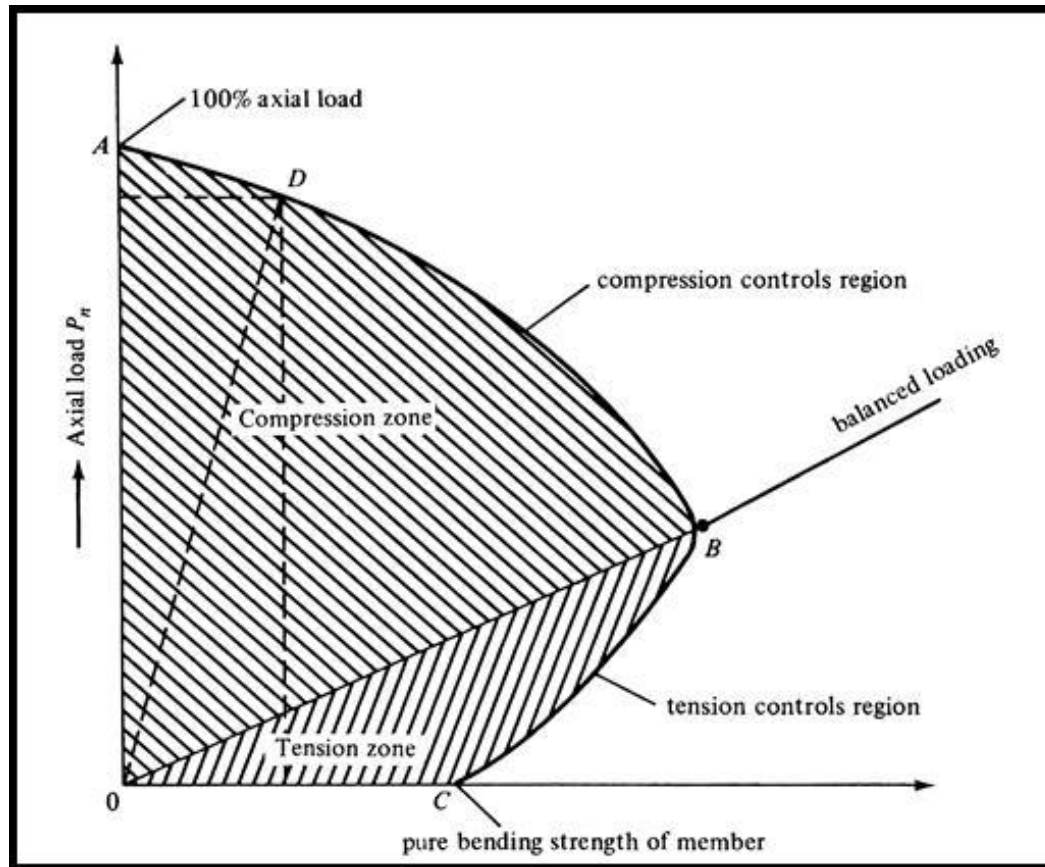
Eccentrically loaded column

OR



Description of Interaction Diagram

2



Normalized Interaction Diagrams

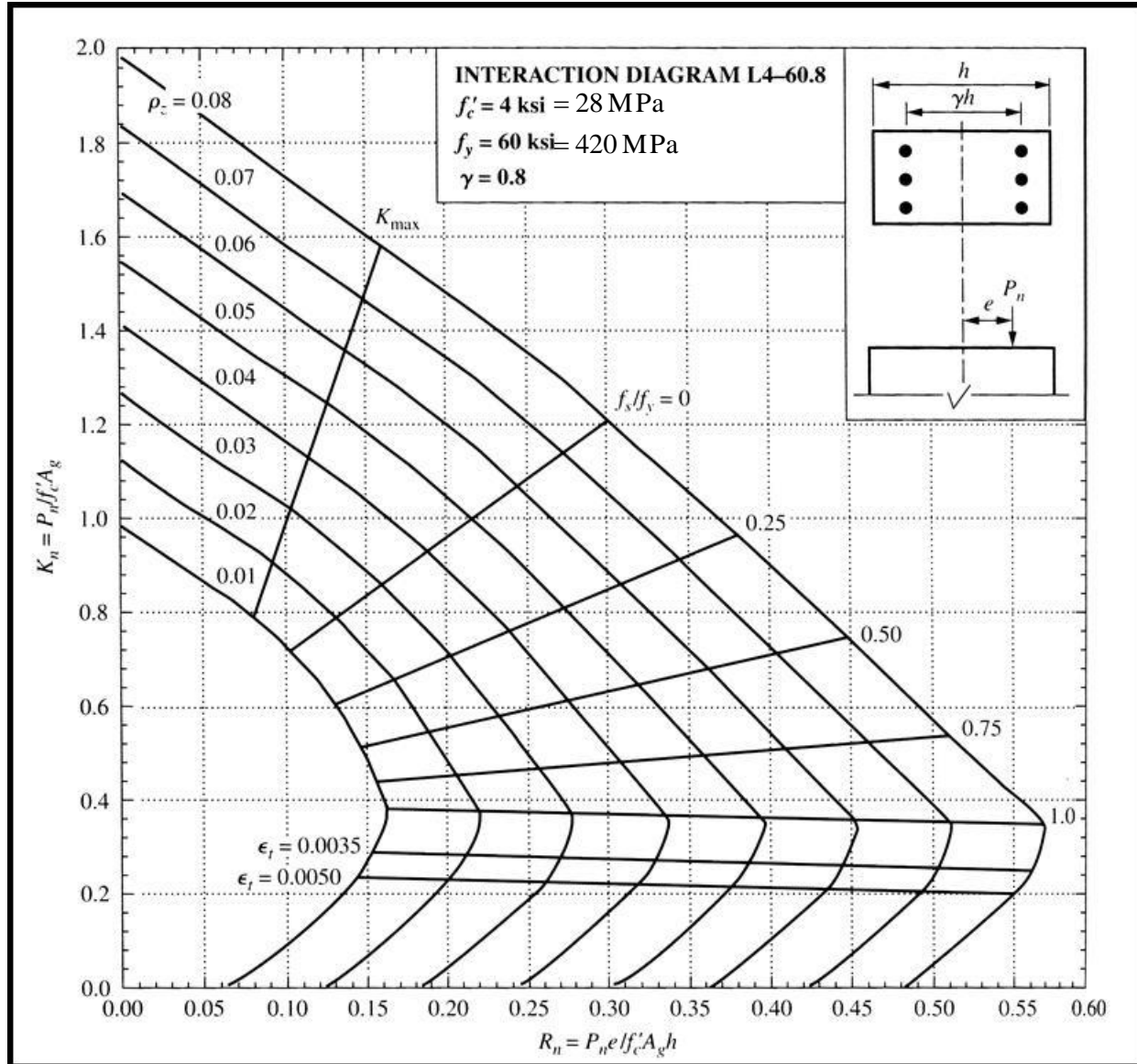
3

If the diagrams are plotted with ordinates of K_n (instead of P_n) and R_n (instead of M_n), defined below, the resulting normalized diagram can be used with any system of units.

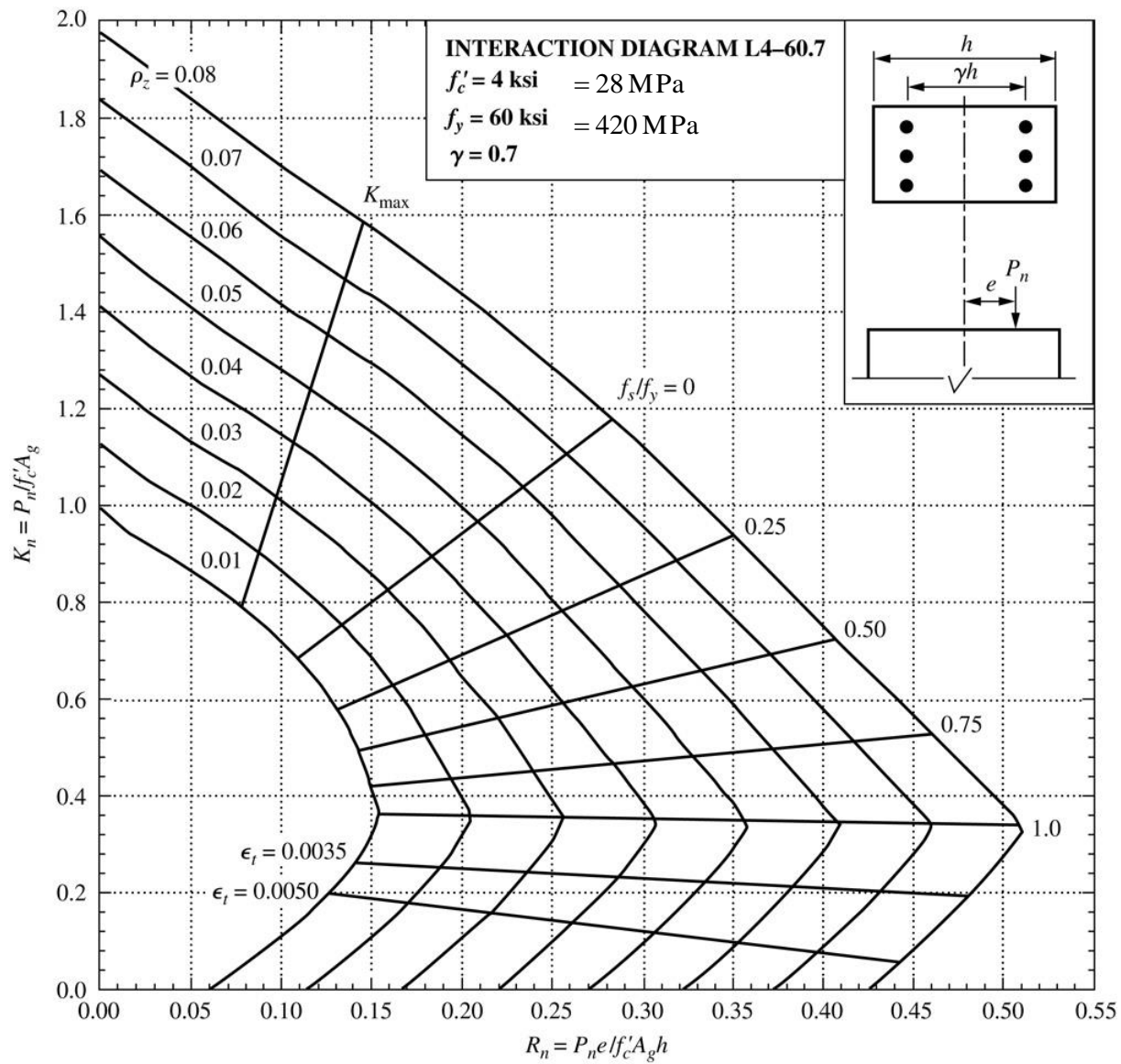
$$K_n = \frac{P_n}{f_c' A_g}$$

$$R_n = \frac{P_n e}{f_c' A_g h}$$

A sample Column Interaction Diagram



γ = distance from the center of the bars on one side of the column to the center of the bars on the other side of the column divided by h .



Problem-1

6

Design a short square tied column for the following loads: $P_u = 2700$ kN and $M_U = 112$ kNm. Place the bars uniformly around all four faces of the column. The concrete strength is 28 MPa and the steel is Grade 420. If $V_u = 56$ kN, check the designed column for shear.

Solution

7

Column Dimensions

$$A_{g(\text{trial})} \geq \frac{P_u}{0.40(f'_c + f_y \rho_t)}$$

Assume:

$$\rho_t = 2\%$$

$$A_g = h^2 \Rightarrow h = \sqrt{A_g} = 430\text{mm}$$

Selecta 400 × 400 mm column ($A_g = 160000 \text{ mm}^2$)

$$\phi P_n = P_u = 2700 \text{ kN} \Rightarrow P_n = 2700 / \phi = 2700 / 0.65 = 4153.9 \text{ kN}$$

$$\phi M_n = M_u = 112 \text{ kNm} \Rightarrow M_n = 112 / \phi = 112 / 0.65 = 172.3 \text{ kNm}$$

$$M_n = P_n e \Rightarrow e = \frac{M_n}{P_n} = \frac{172.3}{4153.9} = 0.04147 \text{ m} \Rightarrow e = 41.47 \text{ mm}$$

Parameters required to use the interaction diagrams

8

$$K_n = \frac{P_n}{f_c' A_g} = \frac{4153.9 \times 1000}{28 \times (400 \times 400)} = 0.927$$

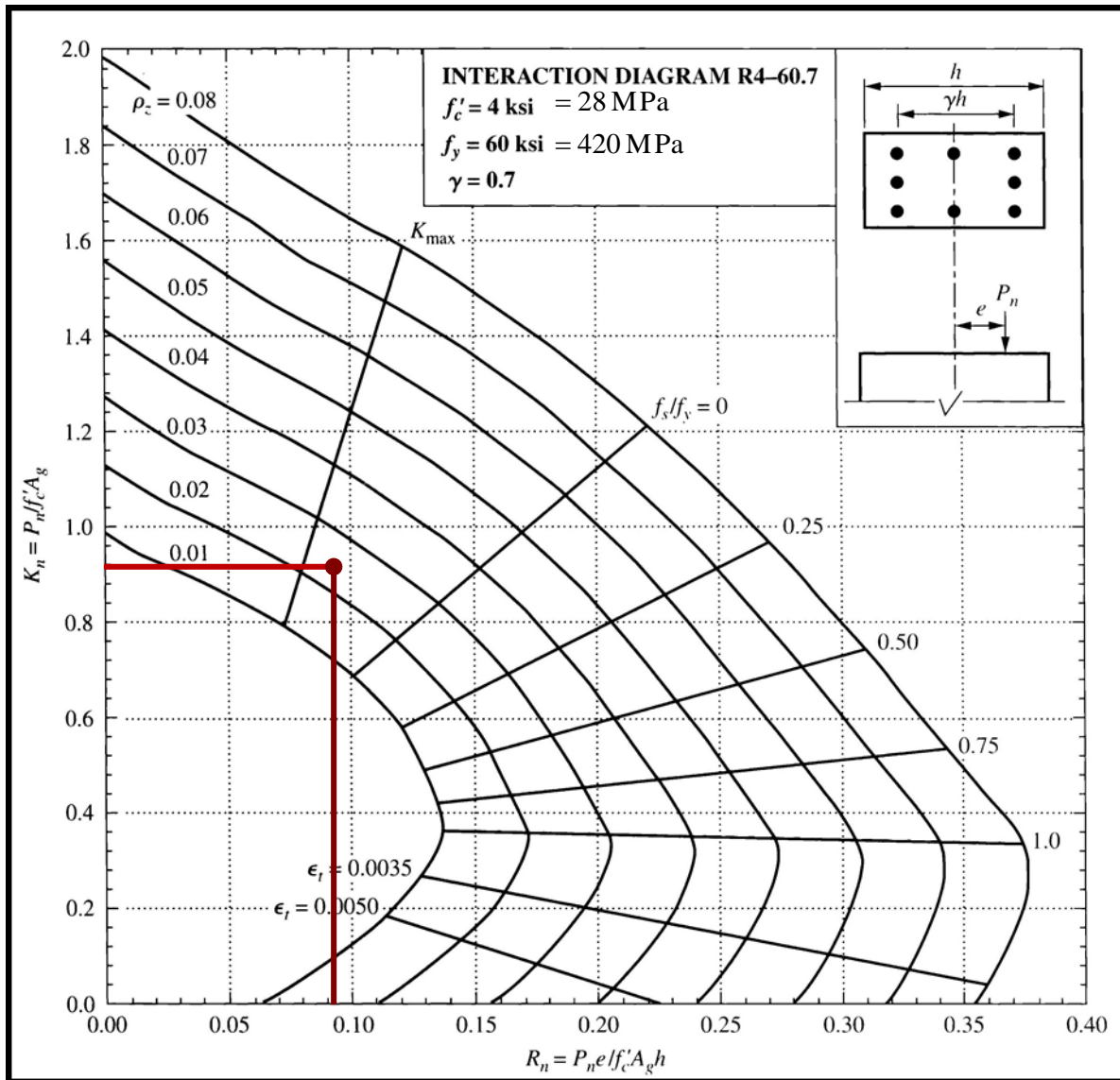
$$R_n = \frac{P_n e}{f_c' A_g h} = \frac{4153.9 \times 1000 \times 41.47}{28 \times (400 \times 400) \times 400} = 0.096$$

Let us assume the effective cover = 60 mm

Effective cover = Clear cover + d_s + $0.5d_b$ = 60 mm (say)

$$\gamma = \frac{\gamma h}{h} = \frac{h - 2 \times \text{Effective cover}}{h}$$

$$\Rightarrow \gamma = \frac{400 - 2 \times 60}{400} = 0.7$$



$$K_n = 0.927$$

$$R_n = 0.096$$

$$\gamma = 0.70$$

$$\rho_g = 0.024$$

Point is in
the compression zone
 $\Rightarrow \phi = 0.65$ OK.

Contd.

10

$$\rho_g = \frac{A_s}{A_g} \Rightarrow A_s = \rho_g A_g = \rho_g bh$$

$$\Rightarrow A_s = 0.024 \times 400 \times 400 = 3840 \text{ mm}^2$$

$$\text{Number of bars} = \frac{A_s}{A_b} = \frac{3840}{491} = 7.8 \approx 8 \text{ bars}$$

Use 8 - 25 mm bars ($A_s = 8 \times 491 = 3928 \text{ mm}^2$)

Contd.

11

Design of Ties (Assuming 10 mm ties)

Minimum Tie Size = 10 mm for long. bars of size
less than 32 mm. OK

Spacing : Vertical spacing (pitch) of ties shall not exceed :

(a) $16 \times$ longitudinal bar diameter = $16 \times 25 = 400$ mm

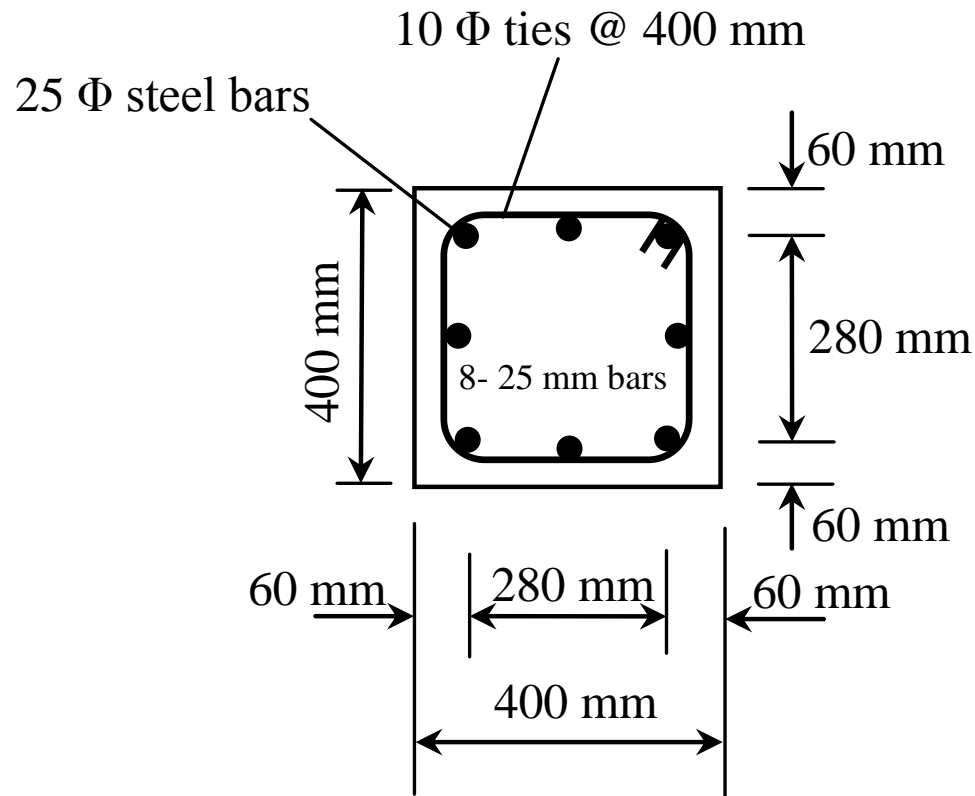
(b) $48 \times$ tie bar diameter = $48 \times 10 = 480$ mm

(c) Least dimension of the column section = 400 mm

Use 10 mm ties at 400 mm c/c

Sketch of the Column Cross section

12



Check for shear

13

$$V_u = 56 \text{ kN}$$

$$d = h - (\text{cover} + \frac{d_b}{2} + d_s) = 400 - 60 = 340 \text{ mm}$$

$$b_w = 400 \text{ mm}$$

$$V_c = \left(1 + \frac{P_u}{14A_g}\right) \frac{\sqrt{f'_c}}{6} b_w d = \left(1 + \frac{2700 \times 1000}{14 \times (400 \times 400)}\right) \frac{\sqrt{28}}{6} \times 400 \times 340$$

$$\Rightarrow V_c = 264512 \text{ N} = 264.5 \text{ kN}$$

$$0.5\phi V_c = 0.5 \times 0.75 \times 264.5 = 99.2 \text{ kN}$$

Since $0.5\phi V_c > V_u (= 56 \text{ kN})$ OK

